

THERMODYNAMICS DETAILS

FOUNDATIONS ARE BASED ON EMPIRICAL OBSERVATIONS
⇒ LAWS

- I) 1ST LAW CONSERVATION OF ENERGY
1st IN ANY PROCESS ENERGY IS CONSERVED
- $$dE = \delta W + \delta Q$$
- $E \Rightarrow$ total energy $\Rightarrow dE$ variation of energy
due by some process
- $W \Rightarrow$ MECHANICAL WORK $\Rightarrow \delta W$ mechanical work
done on the system
- $Q \rightarrow$ HEAT $\Rightarrow \delta Q$ heat given to
the system.

Why dE & δW ? What is the difference between
 $d(\cdot)$ & $\delta(\cdot)$? FUNDAMENTAL!

E is a function of state of the system (x)

\Rightarrow going from x_0 to x_1 (states)
is function only on FINAL & INITIAL
position, not path!!!

$$\Delta E = \int_{x_0}^{x_1} dE$$


DOES NOT
DEPEND ON
PATH

$$\Rightarrow \Delta E(\text{closed loop}) = \int_{x_0}^{x_0} dE = 0$$


CHANGE OF A STATE FUNCTION ON A
REVERSIBLE PROCESS IS ZERO

T1

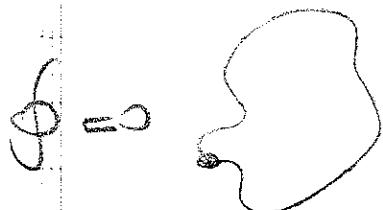
IN MATHEMATICAL TERMS

d = DIFFERENTIAL

EXAMPLE $f(x, y)$ = STATE FUNCTION
 (x, y) STATE

DIFFERENTIAL $df = \frac{\partial E}{\partial x} dx + \frac{\partial E}{\partial y} dy$

$\stackrel{?}{\partial^2 f}$ $\frac{\partial^2 f}{\partial x \partial y}$ $\frac{\partial^2 f}{\partial y \partial x}$, are they identical?
 IF $\frac{\partial^2 f}{\partial x \partial y} = \frac{\partial^2 f}{\partial y \partial x} \Rightarrow f$ is
 CALLED
 CLOSE FORM.



$\oint df = 0$ integral on
 loop a loop $= 0$



$\int_{(x_0, y_0)}^{(x_1, y_1)} df =$ does NOT depend
 on path

$\Rightarrow dE$ is differential of E
 $\& E$ is a function of state (for the 1st law)

T2

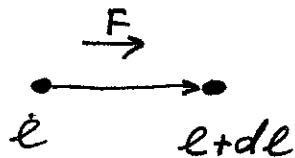
What about δ ?

δ represents a tiny ^{Variation} ~~assort~~ of something but it's not a differential!!!

$\delta \neq d$
no DIFF

EXAMPLE

$\delta W =$ tiny amount of work to go from close states

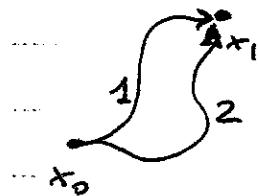


$$\delta W = F dl$$

δW is not differential of W !!

$$W = FR \quad \text{||}$$
$$dW = d(FL) = Fdl + Ldf \quad \text{||}$$
$$\delta W = F dl \quad \text{NOTHING}$$

δ (SOMETHING)^{symbol} is applied when the variation depends on the path



& $\delta Q_1 \neq \delta Q_2$ depends on the path, the way you go from 1 to 2

so $dF = \frac{\partial F}{\partial x} dx + \frac{\partial F}{\partial y} dy \Rightarrow$ if $\frac{\partial^2 F}{\partial x \partial y} \neq \frac{\partial^2 F}{\partial y \partial x} \Rightarrow$

PATH DEPENDENCE \Rightarrow
need δ & not d

USUALLY CALLED

d = PERFECT DIFFERENTIAL, DIFFERENTIAL ... FOR STATE FUNCTIONS
 δ = DELTA, VARIATION OF, ... FOR NO-STATE FUNCTIONS!

T3

we know

$$\delta W = -pdV$$

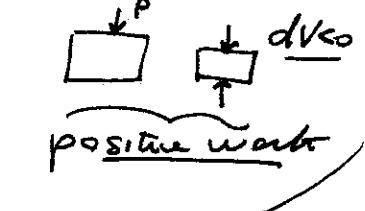
(— because if V decreases with position we have to move work

V is a state function!! $\Rightarrow dV$

of course, V is a state variable by itself.

$$\Rightarrow dE = \underbrace{-pdV}_{\text{comes from } -PV} + \delta Q$$

$$H \equiv E - (-PV) = E + PV$$



(Legendre transformation

= subtract conjugate variables

$$\Rightarrow dH = Vdp + \delta Q$$

ENTHALPY, at constant pressure, contains HEAT VARIATION!!

$$dH|_P = \delta Q \Rightarrow$$

EXPERIMENT:

IN OPEN AIR (CONSTANT 1 ATM)

RAISE TEMPERATURE OF

ONE SOLID \Rightarrow MAKE ΔH
NOT ΔE !!

$$\delta Q = dH|_P = dE|_V$$

$$C \equiv \frac{\delta Q}{\delta T}$$

specific heat: how much heat to give to raise temp of 1 degree

$$C_p = \left. \frac{\delta Q}{\delta T} \right|_P = \left. \frac{dH}{dT} \right|_P$$

$$C_v = \left. \frac{\delta Q}{\delta T} \right|_V = \left. \frac{dE}{dT} \right|_V$$

USE H to describe systems @ $P=\text{const}$
NOT E

T4

II)

S_Q IS NOT A FUNCTION OF STATE BUT

THERE IS A STATE FUNCTION, S. ENTROPY, FOR WHICH
FOR ALL REVERSIBLE PROCESSES AND ALL IRREVERSIBLE PROCESSES

$$dS = \frac{S_Q_{\text{ref}}}{T}$$

$$dS > \frac{S_Q}{T}$$

EQUILIBRIA ARE NOT ALWAYS REVERSIBLE

REV. OF EQ: SMALL VARIATION TAKEN & GIVEN BACK BRINGS TO THE SAME POINT

\Rightarrow IF IN A CLOSE LOOP



I GET SOME EXTRA ENTROPY \Rightarrow THIS MEASURES DEGRADATION

(MORE HEAT EXCHANGE \Rightarrow MORE ENTROPY)

$$\Rightarrow dE = -pdV + Tds$$

ENERGY

$$dH = Vdp + Tds$$

$H = E + PV$ ENTHALPY

$$dA = -pdV - SdT$$

$A = E - ST$ (HELMOLZ)

good @ V, T constant

$$dG = -Vdp - SdT$$

$G = E + PV - ST$ (GIBBS)

good @ P, T constant

Like normal Life

(TOTAL ENTROPY OF UNIVERSE \uparrow)

TS

III)

STABILITY? WHAT TO MINIMIZE?

SECOND LAW IRREV. REV $TdS \geq \delta Q$ IF IRR
 $\delta Q \leq TdS$
 ↑
 IF REV

A VARIATION δ (NOT A DIFFERENTIAL)

$$dE = \delta W + \delta Q \leq SW + TdS$$

$$\Rightarrow dE - SW - TdS \leq 0 \quad \text{suppose } \delta W = -pdV \text{ for much work}$$

$$dE + pdV - TdS \leq 0 \quad \text{FOR ALL} \quad \underline{\text{IRREVERSIBLE PROCESSES}}$$

PROCESS = SOMETHING MOVING $\delta Q \leq TdS$, IRR $\delta Q < TdS$

IF EQUILIBRIUM, NO PROCESS $\Rightarrow \delta Q \geq T\delta S$

\Rightarrow ad equilibrium (variation back/forth does not change state) Virtual Variation
 if you vary $S \rightarrow S'$, you need to violate THE irreversible process
 (because you need to come back)



$$\Rightarrow S' - S \leq \delta Q/T$$

↓
 VIRTUAL VARIATION

APPLIES TO STATE FUNCTIONS TOO

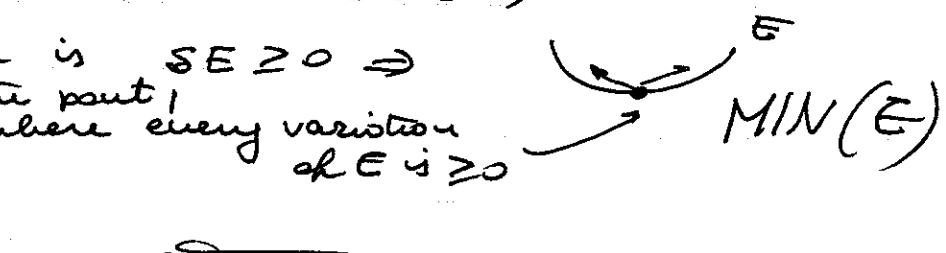
$$\Rightarrow SE - T\delta S + p\delta V \geq 0 \Rightarrow$$

$\downarrow \quad \downarrow \quad \delta Q$

$$SZ = SE - T\delta S + p\delta V \geq 0$$

EQUILIBRIUM

T6

\Rightarrow at $T=0$, constant value \Rightarrow equilibrium is $SE \geq 0 \Rightarrow$ (the point where every variation of E is ≥ 0) 

What about H ? ENTHALPY (IF NO EXTRA HEAT MOVES $SQ=0$)
 $dH = dE + Vdp + Tds$ $Tds=0$

$$\frac{dH}{S} = Vdp \Rightarrow \frac{dH}{S, P} = 0$$

(*) $SZ|_{S, P} = \underbrace{(SE - TSS + PSV)}_{\geq 0 \text{ always}}|_{SP} = (SE + PSV)|_{SP} =$

at constant P ~~$SSE = 0$~~ $\Rightarrow VSP = 0 \Rightarrow$
 $= (SE + PSV + \cancel{VSP})|_{SP} = S(E + PV)|_{SP} = SH_{SP}$

$$\Rightarrow SZ \geq 0 \Rightarrow SH_{SP} \geq 0$$

FOR G ?

$$dG = Vdp - SdT \Rightarrow SZ \geq 0 \Rightarrow SG_{P, T} \geq 0$$

If you like
at T, P const \Rightarrow need to  NOT $\in \dots$

T7

||||)

MELTING \Rightarrow where the HEAT OF MELTING GOES?

$T=0$

SOLID

CONST PRESSURE!

~~$\Delta Q \Rightarrow$~~ $Q \Rightarrow$ SOLID $T \uparrow$

$Q \Rightarrow$ SOLID $T \text{ const}$

$Q \Rightarrow$ LIQUID $T \text{ const}$

$Q \Rightarrow$ LIQUID $T \uparrow$

ΔQ to MELT?

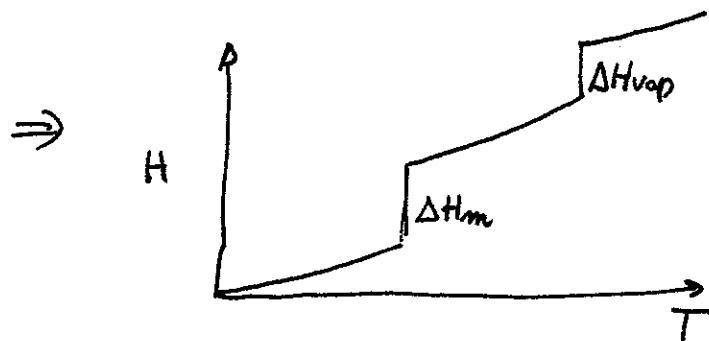
Melt happens at const T

$$dE = -pdV + \cancel{Tds} = \delta Q$$

$$dH = Vdp + \delta Q \quad \text{at } P=\text{const} \quad dH_p = \delta Q$$

$$\Rightarrow \Delta Q_{\text{MELTING}} = \frac{\Delta H_p}{\text{measurable}}$$

$$\Rightarrow T_m \Delta S_m = \Delta H_m \Rightarrow \Delta S_m = \frac{\Delta H_m}{T_m}$$



T8

WHERE S COMES FROM?

F, L, P, V, T, N, are all easy to measure!

where S comes from? What is ~~the~~ It's functional slope?

2nd law tells that

S is function of state
⇒ $\delta S = \frac{\delta Q}{T}$!!

INTENSIVE PROPERTIES:

T, P, F ... properties and quantities that do not depend on the size of the system

EXTENSIVE PROPERTIES

E, Q, S, V ... depend on the size!

EXAMPLE: 1kg of ~~water~~ WATER @ 100° contains E^{∞} JOUCHES ⇒

3kg of WATER @ 100° contains $3 \cdot E^{\infty}$ JOUCHES!

⇒ Energy is Extensive, Volume too (obvious)
Heat too (\Rightarrow therefore S)

IN THERMODYNAMICS

INTENSIVE & EXTENSIVE ARE ASSOCIATED

$$\begin{array}{ccc} -PdV & \downarrow & TdS \\ \text{Int} & \text{Ext} & \downarrow \\ \text{Int} & \text{Ext} & \text{of so on} \end{array}$$

Tg

Q is extensive $\Rightarrow S$ is extensive.

BOLTZMANN IDEA

1) at constant Energy the system can be in $\Omega(E)$ number of states (DEFINITION)

2) all states are equiprobable (ASSUMPTION)
(why a state should be more probable?)

3) $\textcircled{1} + \textcircled{2} \Rightarrow P_E(\tilde{x}) = \frac{1}{\Omega(E)}$ | for every state,

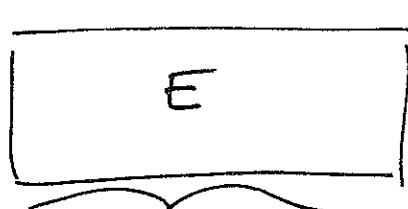
all are $\Omega(E)$
 $\Rightarrow \sum_{\tilde{x} \in \Omega(E)} P_E(\tilde{x}) = 1$

o) BOLTZMAN SAYS

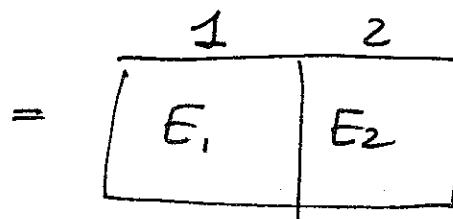
ENTROPY MEASURES THE PROBABILITY DISTRIBUTION

$$S(E) = f_{\text{inv}}(P_E(\tilde{x})) = f(\Omega(E))$$

BUT S is EXTENSIVE \Rightarrow TAKE SYSTEM OF ENERGY E & CUT IN TWO $\Rightarrow E_1, E_2$



$$S(E) = f(\Omega(E))$$



$$E_1 + E_2 = E$$

$$S_1(E_1) = f(\Omega(E_1)) \quad S_2 = f(\Omega(E_2))$$

but the 1 has $\Omega(E_1)$ states & 2 has $\Omega(E_2)$ states,
then 1 + 2 has a total of $\Omega(E_1) * \Omega(E_2)$ possible configurations
TIP (for every one of one, pick one of the other)

$$\Rightarrow \mathcal{D}(\epsilon_1 + \epsilon_2) = \mathcal{D}(\epsilon_1) * \mathcal{D}(\epsilon_2) \quad \text{obvious.}$$

$$\Rightarrow f(\mathcal{L}_1(\epsilon_1) * \mathcal{R}(\epsilon_2)) = f(\mathcal{L}(\epsilon_1)) + f(\mathcal{R}(\epsilon_2))$$

which function has this property?

$$f(a+b) = f(a) + f(b) \quad ?$$

$$\Rightarrow S(E) \propto \log \Omega(E) \Rightarrow S(E) = k_B \log \Omega(E)$$

↑

to get Joules
after multiplying
for T

DEFECTS (FRENKEL)

$$N_I = N_A \exp \left(-\frac{Q_H}{RT} \right)$$

$\Rightarrow N_A$ sites

N_I possible defects \Rightarrow

choose N_I on a set of N_V places

~~All~~ $\rightarrow \text{2} = {}^{\#} \text{choose } N_{\text{I}} \text{ identical defects}$

on a set of N_A identical places

$$\frac{N_A!}{N_I! (N_A - N_I)!}$$

identical places the contours
 N_A identical defects
 & $(N_A - N_I)$ identical
 good places

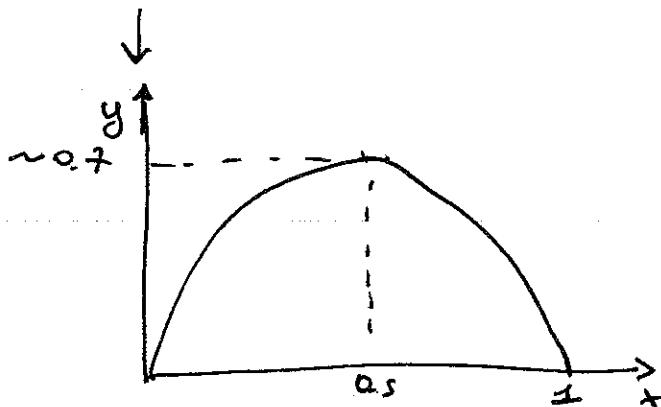
TII

and remember Sterling $\log n! \sim n \log n - n$
 and $x \equiv \frac{N_E}{N_A}$

$$\Rightarrow S = -kN_A [x \log x + (1-x) \log(1-x)]$$

No defect: how many choices? $1 \Rightarrow \mathcal{S} = 0$
 All defects: how many choices? $1 \Rightarrow \mathcal{S} = 0$

$$y = -[x \log x + (1-x) \log(1-x)]$$



To form FRENKEL. (how double occupancy)

I TOOK
 THIS !!

$$\text{so } N_E = N_A e^{-\frac{E_Q}{2kT}}$$

$$\Rightarrow \frac{E_Q}{2kT} = -\log x$$

IS
 THIS TRUE ??

$$Q = -2kT \log x$$

MUST PROVE !

T12

$T, P, \text{const} \Rightarrow \min G!$

$$G = E - TS + PV$$

$$\delta T, \delta P = 0$$

$$\Delta G = \Delta E - T\Delta S + P\Delta V$$

defects do not change volume !!

$$\Delta G = \Delta E - T\Delta S =$$

\rightarrow

$\frac{Q}{2}$ because every Φ gets 2 defects
 $\Rightarrow \frac{Q}{2}$ per defect

$$N_A x \Rightarrow \Delta G = N_A \left[x \frac{Q}{2} - T \Delta S(x) \right]$$

$$\downarrow \\ S(x) - S(0) = S(x)$$

$$\Rightarrow N_A \left[x \frac{Q}{2} + KT \left[x \log x + (1-x) \log(1-x) \right] \right]$$

suppose few $\Rightarrow x \approx 0 \approx 0$ $\Rightarrow (1-x) \log(1-x)$

$\Rightarrow \min \Delta G \Rightarrow \min \Delta G$ over all possible configuration
 $\{x\}$

$$\Rightarrow \frac{\partial \Delta G}{\partial x} = 0$$

$$\Rightarrow \frac{\partial}{\partial x} \left[x \frac{Q}{2} + KT \left[x \log x + (1-x) \log(1-x) \right] \right]$$

$$\Rightarrow \cancel{x} \frac{Q}{2} + KT \log x + KT \cancel{x} \cancel{-} - KT \log(1-x) + \cancel{(1-x)} \cancel{(-1)} \cancel{KT}$$

$$0 = \frac{Q}{2} + KT \log x - KT \log(1-x) = 0$$

$\underbrace{\approx 1}_{\approx 0}$

$$\Rightarrow -\frac{Q}{2KT} \log x \Rightarrow \boxed{N_0 = N_A e^{-\frac{Q}{2KT}}}$$

EQ CONCENTRATION

T13